

1 **The Influence of Motion Control, Neutral and Cushioned Running Shoes on Lower Limb**
2 **Kinematics**

3

4 **Abstract**

5 To-date there is a paucity of information about how different types of conventional running
6 shoes influence lower limb kinematics. The aim of the study was to determine the influence of
7 motion control, neutral and cushioned running shoes upon lower limb kinematics. Twenty-
8 eight active males completed one test session running in standardised motion control, neutral
9 and cushioned running shoes, on a treadmill at a self-selected pace ($2.9 \pm 0.6 \text{ m}\cdot\text{s}^{-1}$). Kinematic
10 data were collected using a VICON motion analysis system with hip, knee and ankle joint
11 angles calculated. Discrete parameters associated with stance phase kinematics were compared
12 between footwear conditions. Significant ($p < .05$) differences in knee flexion and internal
13 rotation at toe off, and knee adduction range of motion were reported between footwear
14 conditions. Significant ($p < .05$) differences in ankle joint dorsi-flexion and adduction upon
15 initial contact, peak dorsi-flexion, eversion and abduction, and inversion at toe off were
16 reported between footwear conditions. The influence of motion control, neutral and cushioned
17 running shoes on joint function dissipates moving proximally, with larger changes reported at
18 the ankle compared to knee and hip joints. While significant differences were reported between
19 footwear conditions, these changes were of a small magnitude and effect size.

20 **Key Words:** footwear, hip, knee, ankle

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22 **Word Count:** 2,934 words

24 Traditional running-injury paradigms have been challenged within the literature¹, yet
25 still underpin running shoe design. As such, running shoes are still designed with stability and
26 cushioning features which are thought to influence the rate and/or magnitude of foot motion
27 and impact loading^{2,3}. Running shoes are often categorised based upon their design features
28 and may broadly be classified as trail, performance, minimalist or conventional running shoes⁴
29 ⁶. Conventional running shoes are often further sub-classified based upon their specific stability
30 and cushioning features, in to motion control, neutral and cushioned categories⁴⁻⁶. Currently no
31 objective method for this sub-classification exists and as such running shoes are often classified
32 based upon manufacturer recommendations. Furthermore, these terms are by no means uniform
33 with different manufactures, retailers or publications often using neutral/stability or
34 cushioned/neutral interchangeably⁴⁻⁸. For clarity the terms motion control, neutral and
35 cushioned will be used exclusively throughout this manuscript. Motion control running shoes
36 aim to reduce the magnitude and/or rate of pronation with a view to enhancing the propulsive
37 efficiency of the foot, in comparison to neutral and cushioned shoes^{6,9,10}. In contrast, cushioned
38 running shoes aim to reduce the magnitude and/or rate of impact loading, and increase foot
39 motion relative to neutral and motion control running shoes^{6,9,10}. Neutral running shoes
40 combine a number of motion control and cushioning features with a view to providing some
41 additional stability compared to cushioned running shoes, and greater force attenuation than
42 motion control running shoes^{6,9,10}.

43 Studies^{11,12} have demonstrated that motion control running shoes reduce rearfoot
44 eversion compared to neutral shoes. However, as is common within footwear biomechanics,
45 these studies^{11,12} placed markers on the shoe. Discrepancies between the motion of the foot and
46 the shoe have been reported¹³⁻¹⁵ and as such, the findings of studies using shoe based markers

47 should be interpreted with caution. The only study¹⁰ known to the authors comparing in-shoe
48 foot motion, when running in motion control and cushioned running shoes, found no significant
49 differences in rearfoot eversion. Further work is required to explore the influence of motion
50 control, neutral and cushioned running shoes on in-shoe foot motion.

51 Assessment of rearfoot eversion has been widely reported over the past 40 years^{11,12,17-}
52 ¹⁹ as a measure of how footwear influences foot motion. This approach offers limited
53 understanding of the influence footwear modifications may have upon the sagittal and
54 transverse plane motions of the foot, or upon more proximal joints. The assessment of how
55 footwear influences lower limb kinematics may help to elucidate mechanisms by which injury
56 risk can be mitigated; as hip and knee joint kinematics have been linked to the development of
57 overuse running injuries²⁰⁻²³. Two studies^{10,24} have demonstrated that motion control running
58 shoes reduce internal tibial rotation compared to cushioned or neutral running shoes,
59 respectively. While Hutchison et al²⁵ reported significant reductions in internal knee rotation
60 when running in motion control shoes compared to neutral shoes. These findings highlight that
61 motion control, neutral and cushioned running shoes have the potential to influence more
62 proximal joint kinematics. However, there is a lack of published data relating to the influence
63 of these types of commercially available running shoes upon three dimensional (3D) lower
64 limb kinematics. The aim of this study was to determine the influence of motion control, neutral
65 and cushioned running shoes on lower limb kinematics. Three hypotheses were tested; (1)
66 lower limb kinematics will differ between motion control, neutral and cushioned running shoes,
67 (2) motion control running shoes will reduce the magnitude of ankle joint eversion compared
68 to neutral and cushioned running shoes, and (3) cushioned running shoes will increase the
69 magnitude of ankle joint eversion compared to neutral and motion control running shoes.

70

71

Methods

72 Based upon an *a priori* sample size calculation, using the method of Eng²⁶ and the data
73 of Cheung and Ng¹¹, 28 active males (26 ± 7 years, 1.77 ± 0.05 m, 79 ± 9 kg) were recruited
74 for this study. Participants were free from injury and/or illness at the time of testing, as
75 determined by a health screening questionnaire. On average participants reported exercising
76 three to four times per week, including running two to three times per week. Foot strike pattern
77 was not controlled within the study to enhance the generalisability of the findings; 19
78 participants were rearfoot, 6 midfoot and 3 forefoot strikers. Ethical approval was granted for
79 this study by the Research Ethics Committee of the host institution and written informed
80 consent was provided by all participants prior to testing.

81 Participants attended one test session lasting between 1 – 1.5 hours. At the beginning
82 of the session, participants undertook a 10 minute familiarization period on a Jaeger LE 300 C
83 treadmill (Erich Jaeger GmbH & Co, Wuerzburg, Germany), to minimise kinematic
84 differences between overground and treadmill conditions^{27,28}. After the familiarization period,
85 anatomical and tracking markers were attached in line with a four segment lower limb model
86 (described below). An eight camera VICON MX motion analysis system (VICON Motion
87 Systems Ltd., Oxford, England), operating at 200Hz, was used to track the position of retro-
88 reflective markers attached to foot and lower limb. Prior to data collection, the VICON system
89 was calibrated following the manufacturer's guidelines.

90 To define the foot, shank, thigh and pelvis, 14mm retro-reflective markers were
91 attached to the right limb at the following locations; first and fifth metatarsal heads, medial and
92 lateral malleoli, medial and lateral femoral epicondyles, and bilaterally to the anterior and
93 posterior superior iliac spines. In accordance with the calibrated anatomical system technique²⁹,
94 marker clusters were used to track each segment during dynamic trials. The foot was tracked

95 by a triad marker cluster attached to the posterior-lateral aspect of the calcaneus at the height
96 of the Achilles tendon attachment (Figure 1). To enable the marker cluster to be attached
97 directly to the foot, a 25 mm incision was made within each shoe^{30,31}. Four incisions were made
98 within the shoe in total, as this study was part of a larger project which also explored inter-
99 segmental foot kinematics. The incision set was found to have minimal influence upon the
100 running shoes structural integrity³¹. The thigh and shank were tracked by rigid clusters,
101 consisting of four non-collinear markers, located on the distal-lateral aspect of the segment.
102 The pelvis was tracked by a rigid cluster of four non-collinear markers attached to the proximal-
103 posterior aspect of the segment. Once participants were fully fitted with both anatomical and
104 tracking markers a single, static trial was recorded, in a barefoot condition. This enabled the
105 relevant anatomical reference frames to be calculated for each segment. After the static trial
106 was recorded anatomical markers were removed.

107 Participants ran at a self-selected pace ($2.9 \pm 0.6 \text{ m.s}^{-1}$) and completed three minute
108 trials in each of the shod conditions; motion control, neutral and cushioned. Data were collected
109 continuously for the final 30 seconds of each trial. The order of testing was randomised to
110 reduce potential order effects. Footwear was standardised using running shoes provided by the
111 manufacturer and classified according to the manufacturer's advice; motion control (ASICS
112 Gel-Forte), neutral (ASICS GT 2000 2) and cushioned (ASICS Gel-Cumulus 15). Details of
113 the design characteristics of each footwear condition are provided in table 1.

114 Raw marker trajectories were reconstructed, labelled and filtered using a 10Hz
115 Butterworth filter, within VICON Nexus 1.7.1 (Vicon Motion Systems Ltd., Oxford, England).
116 Gaps, of up to five frames, in marker trajectories were filled using the in-built pattern fill
117 function within VICON Nexus 1.7.1. Processed trials were cropped to five consecutive gait
118 cycles and exported to Visual 3D (C Motion Inc., Leicester, England) where 3D hip, knee and

119 ankle joint kinematics were calculated. Gait cycle parameters were identified from the
120 kinematic data³². Joint angles were averaged and time normalised to 100 % stance phase
121 duration. All joint angles were normalised for each participant to their static posture recorded
122 barefoot in a relaxed standing position, enabling differences in absolute joint angles to be
123 compared between footwear conditions³³. Discrete angles were pre-selected, in line with the
124 literature³⁴, to describe the motion pattern of each joint and extracted for statistical analysis.
125 The discrete variables used to describe stance phase kinematics were angles at initial contact
126 (IC) and toe off (TO), joint range of motion (ROM), peak angles and time to peak angle.

127 Descriptive statistics (mean (standard deviation)) were calculated within Microsoft
128 Excel 2013 (Microsoft, Redmond, WA, USA). Statistical analysis was undertaken in SPSS 20
129 (IBM, Armonk, NY, USA). Prior to data analysis, all data were explored for normal distribution
130 using a Shapiro-Wilk test. Where data met parametric assumptions, differences between shod
131 conditions were explored using a one-way repeated measures analysis of variance (ANOVA).
132 Where significant main effects were observed, post hoc pairwise comparisons were undertaken.
133 Where data violated parametric assumptions, differences between shod conditions were
134 explored using Friedman's ANOVA. Where significant main effects were observed, pairwise
135 comparisons were conducted post hoc. Partial eta squared (η^2) was used as an estimate of effect
136 size for the repeated measures ANOVA and Kendall's W (W) was used for Friedman's
137 ANOVA. Effect sizes were interpreted as follows; small effect $\geq .10$, moderate $\geq .30$ and large
138 $\geq .50$ ³⁵. The level of significance for main effect within the study was set at $p < .05$, with post
139 hoc comparisons Bonferroni corrected.

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143 Significant main effects were observed for ankle joint dorsi-flexion upon IC ($p = .01$,
144 $W = .16$) and peak ankle dorsi-flexion in stance ($p = .02$, $W = .14$) (Table 2, Figure 2). The
145 ankle was significantly more dorsi-flexed upon IC by 2.4° and 3.3° when running in the neutral
146 shoe compared to the motion control ($p = .02$) and cushioned shoes ($p = .03$), respectively.
147 Peak ankle joint dorsi-flexion was significantly increased by 2.6° when running in the neutral
148 shoe compared to the cushioned shoe ($p = .02$). In the frontal plane, significant main effects
149 were observed for ankle joint inversion at TO ($p = .05$, $\eta^2 = .11$) and peak ankle joint eversion
150 ($p = .04$, $W = .12$). The ankle was significantly more inverted at TO by 1° when running in the
151 neutral shoe compared to the motion control shoe ($p = .04$), and peak ankle joint eversion was
152 significantly greater by 0.2° in the motion control shoe compared to the cushioned shoe ($p =$
153 $.05$). Significant main effects were reported for ankle joint adduction upon IC ($p = .03$, $\eta^2 =$
154 $.12$) and peak ankle joint abduction ($p = .01$, $\eta^2 = .15$). The ankle joint was significantly ($p =$
155 $.03$) more adducted upon IC when running in the neutral shoe compared to the motion control
156 shoe by 1.4° . Peak ankle joint abduction was significantly ($p = .02$) greater when running in
157 the motion control shoe compared to the neutral shoe by 1.4° .

158 In the sagittal plane at the knee joint, a significant main effect ($p = .04$, $\eta^2 = .17$) was
159 reported for knee flexion upon TO (Table 3, Figure 2). The knee was significantly ($p = .03$)
160 more flexed at TO by 1.1° when running in the neutral shoe compared to the cushioned shoe.
161 A significant main effect ($p = .02$, $W = .14$) for adduction ROM was found. Knee adduction
162 ROM was significantly ($p = .02$) increased in the neutral shoe compared to the cushioned shoe
163 by 0.4° . In the transverse plane, a significant main effect ($p = .04$, $W = .12$) was observed for
164 the magnitude of knee internal rotation at TO. The knee was significantly ($p = .05$) more
165 internally rotated at TO by 0.5° in the motion control shoe compared to the cushioned shoe.

166 No significant ($p > .05$) differences in hip joint kinematic parameters were recorded
167 between footwear conditions (Table 4, Figure 2).

168

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Discussion

170 This study examined the impact of motion control, neutral and cushioned running shoes
171 on 3D lower limb kinematics. The findings of this study support hypotheses one with
172 significant differences reported in both knee and ankle joint movement patterns between
173 footwear conditions (Tables 2 & 3). However, these significant differences are small in terms
174 of both magnitude ($\leq 3.3^\circ$) and effect size ($\leq .17$), and are below the reported minimal
175 detectable difference ($3-6^\circ$) for lower limb kinematics during running³⁶. As such the significant
176 changes must be interpreted with caution.

177 The assessment of hip, knee and ankle joint motion within this study provides a more
178 comprehensive insight into how different types of footwear influence lower limb kinematics,
179 in comparison to single joint assessments typically reported within the literature^{11,24,25}.
180 Statistically significant differences in knee and ankle joint movement patterns, that would be
181 missed by traditional assessments of ankle joint eversion alone, were identified within this
182 study. Furthermore, changes in knee joint kinematics, across all three planes, were reported
183 which further highlight the efficacy of different types of conventional running shoes to
184 influence motion patterns higher up the kinematic chain. The magnitude of change between
185 footwear conditions reduced more proximally within the kinematic chain. A finding that is
186 supported by Lilley et al¹². Additional work undertaken by the authors of this study further
187 supports the suggestion that the influence of running shoes upon joint kinematics reduces as
188 you move proximally up the kinematic chain, with changes of a larger magnitude reported for

189 parameters associated with inter-segmental foot kinematics for the same participants running
190 in the same footwear conditions^{37,38}. As such footwear appears to offer a means of altering foot
191 or ankle joint motion to a greater extent than the movements of the knee or the hip, with the
192 findings of this study suggesting different types of conventional running shoes have little
193 influence on hip joint kinematics.

194 Peak ankle eversion was greater when running in the motion control shoe compared to
195 the cushioned shoe, however both the magnitude of change (0.2°) and the effect size ($W = .12$)
196 were small (Table 2). This finding contrasts with what would be expected from the design aims
197 of each shoe and the previous literature^{11,12}, and rejects hypotheses two and three. Studies^{11,12}
198 using shoe-based markers have reported significant reductions in peak RF eversion of between
199 0.9° and 6.5° when running in motion control shoes compared to neutral shoes. In contrast,
200 Butler et al¹⁰ reported no significant differences in in-shoe foot motion between motion control
201 and cushioned running shoes, suggesting small differences between conditions, however no
202 data was reported by the authors. The disparity between the studies using shoe based
203 markers^{11,12} and those tracking in-shoe foot motion, such as this one, is important. The existing
204 literature suggests that peak shoe eversion is lower in motion control shoes compared to neutral
205 shoes, potentially due to the more rigid heel counter. However, the reduction in peak shoe
206 eversion does not appear to be replicated by the motion of the foot within the shoe. This is
207 supported by Van Gheluwe, et al³⁹ who reported larger discrepancies between in-shoe foot
208 motion and the motion of the shoe with more rigid heel counters, such as those built in to the
209 motion control shoe. It should be noted at this time that the lack of consistency in running shoe
210 classification and design features across studies and manufacturers may also explain some of
211 the disparity between studies.

212 Significant differences between footwear conditions were also reported in the sagittal
213 and transverse planes at the ankle joint (Table 2). Running in the neutral shoe was associated
214 with significantly increased ankle joint dorsiflexion upon IC and peak dorsiflexion. These
215 changes in sagittal plane kinematics are likely due to the decreased rearfoot to forefoot drop of
216 the neutral shoe (Table 1), placing the foot in a more dorsiflexed position compared to the
217 motion control and cushioned shoes. In the transverse plane, ankle abduction upon IC and peak
218 abduction were significantly greater when running in the motion control shoe compared to the
219 neutral shoe (Table 2). Visual assessment of Figure 2 reveals that the foot is in a more abducted
220 position throughout the entire stance phase when running in the motion control shoe compared
221 to the neutral and cushioned shoes. Closer inspection of the motion patterns reveals that the
222 difference between the three footwear conditions reduces as the stance phase progresses. As
223 such it is speculated that differences in the construction of the rearfoot and midfoot sections of
224 the shoe are liable to account for differences in transverse plane ankle joint motion between
225 footwear conditions.

226 There are a number of limitations that must be acknowledged. The use of a single model
227 and manufacturer for each type of shoe may limit the ability to extrapolate the findings of this
228 study beyond running shoes highly similar to those assessed, due to differences in shoe
229 construction between models/manufacturers. The lack of any mechanical testing to quantify
230 the properties of the respective midsoles of each footwear condition further limits the ability to
231 compare to alternative shoe models. However, previous studies^{11,12} have not provided this
232 information. Additionally, the lack of a prolonged habituation period to each footwear
233 condition may mean that the findings represent only the acute adaptations to each type of
234 running shoe.

235 The findings of this study demonstrate that different types of conventional running
236 shoes significantly influence knee and ankle joint kinematics during the stance phase of running
237 gait, thus supporting hypotheses one. However, while there are significant differences between
238 the motion control, neutral and cushioned running shoes the magnitude of change ($\leq 3.3^\circ$) and
239 effect sizes ($\leq .17$) were small. Surprisingly, based upon the findings of previous studies^{11,12}
240 and the design aims of the respective shoes, motion control shoes did not reduce peak ankle
241 joint eversion. The discrepancies between the findings of this study and the literature may be
242 explained by the assessment of in-shoe foot motion, within the present work. This finding also
243 questions the recommendation of motion control running shoes with a view to reducing the
244 magnitude of foot eversion with a view to reducing injury risk.

245

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249

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341

342 **Tables and Legends**

343

344 Table 1. Design characteristics of the motion control, neutral and cushioned shoes used within
 345 this study

| | Motion Control | Neutral | Cushioned |
|-------------------------------------|-----------------------|----------------|------------------|
| Weight (g) | 377 | 312 | 329 |
| Forefoot Height (mm) | 27 | 25 | 26 |
| Rearfoot Height (mm) | 39 | 34 | 37 |
| Heel-Toe Drop (mm) | 12 | 9 | 11 |
| Impact Guidance System | X | X | X |
| Guidance trusstic system | | | X |
| Reinforced guidance trusstic system | X | X | |
| Rearfoot Gel Cushioning System | X | X | X |
| Forefoot Gel Cushioning System | X | X | X |
| Duomax Support System | X | X | |
| Triple density midsole | X | | |
| FluidRide EVA Midsole | | X | |
| Guidance Line | X | X | X |
| SpEVA 45 lasting | | | X |
| SpEVA 55 lasting | | X | |
| SpEVA 65 Lasting | X | | |
| Broader Sole Plate | X | | |
| Heel Counter | X | X | X |
| Heel Counter Reinforcement | X | | |
| Sotyle EVA midsole | X | | X |

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347

348 Table 2. Comparison of ankle joint kinematic parameters (mean (SD)) in motion control,
 349 neutral and cushioned running shoes

| | Motion Control | Neutral | Cushioned |
|--|----------------|-------------|-------------------------|
| X (+ = Dorsi- / - = Plantar) | | | |
| Angle at initial contact (°) | -2.8 (6.2) | -0.4 (7.4)* | -3.7 (8.9) [†] |
| Angle at toe off (°) | -21.6 (9.3) | -20.1 (8.7) | -23.3 (11.5) |
| Range of motion (°) | 37.6 (7.7) | 37.9 (7.7) | 38.5 (7.7) |
| Peak dorsi-flexion (°) | 16.0 (5.6) | 17.8 (7.8) | 15.2 (8.0) [†] |
| Time to peak dorsi-flexion (sec) | 0.11 (0.02) | 0.11 (0.02) | 0.11 (0.02) |
| Y (+ = Inversion / - = Eversion) | | | |
| Angle at initial contact (°) | 1.5 (3.8) | 1.6 (4.4) | 1.9 (4.8) |
| Angle at toe off (°) | 4.5 (4.8) | 5.5 (5.0)* | 4.8 (5.9) |
| Range of motion (°) | 12.4 (3.0) | 12.9 (3.2) | 12.6 (3.5) |
| Peak eversion (°) | -7.7 (4.2) | -7.2 (4.6) | -7.5 (6.0)* |
| Time to peak eversion (sec) | 0.07 (0.02) | 0.08 (0.03) | 0.07 (0.02) |
| Z (+ = Adduction / - = Abduction) | | | |
| Angle at initial contact (°) | 0.3 (3.9) | 1.7 (4.3)* | 1.7 (5.0) |
| Angle at toe off (°) | -1.0 (4.9) | -0.2 (5.0) | -0.1 (5.6) |
| Range of motion (°) | 7.7 (2.9) | 7.6 (3.6) | 7.7 (3.6) |
| Peak abduction (°) | -5.1 (3.8) | -3.8 (4.5)* | -3.8 (4.8) |
| Time to peak abduction (sec) | 0.06 (0.05) | 0.11 (0.09) | 0.08 (0.08) |

350 * Significantly different to motion control

351 [†] Significantly different to neutral

352 Table 3. Comparison of knee joint kinematic parameters (mean (SD)) in motion control, neutral
 353 and cushioned running shoes

| | Motion Control | Neutral | Cushioned |
|---|----------------|-------------|-------------------------|
| X (+ = Flexion/ - = Extension) | | | |
| Angle at initial contact (°) | 15.1 (7.9) | 16.0 (8.2) | 15.4 (6.5) |
| Angle at toe off (°) | 13.7 (5.2) | 14.1 (5.3) | 13.0 (5.7) [†] |
| Range of motion (°) | 24.7 (3.8) | 24.0 (4.2) | 24.2 (4.5) |
| Peak flexion (°) | 36.7 (6.5) | 37.0 (6.7) | 36.4 (6.5) |
| Time to peak flexion (sec) | 0.09 (0.01) | 0.08 (0.02) | 0.09 (0.01) |
| Y (+ = Adduction/ - = Abduction) | | | |
| Angle at initial contact (°) | -0.2 (3.5) | -0.1 (3.6) | -0.1 (3.1) |
| Angle at toe off (°) | 0.3 (3.5) | 0.4 (3.6) | 0.5 (3.5) |
| Range of motion (°) | 4.3 (1.9) | 4.6 (2.3) | 4.2 (2.0) [†] |
| Peak abduction (°) | -2.8 (3.2) | -3.0 (3.2) | -2.7 (2.9) |
| Time to peak abduction (sec) | 0.10 (0.07) | 0.09 (0.06) | 0.08 (0.05) |
| Z (+ = Internal/ - = External) | | | |
| Angle at initial contact (°) | 4.5 (4.1) | 4.5 (5.0) | 4.5 (3.9) |
| Angle at toe off (°) | 1.2 (3.9) | 1.0 (3.9) | 0.7 (3.6)* |
| Range of motion (°) | 11.9 (4.5) | 12.1 (4.3) | 12.1 (4.3) |
| Peak internal rotation (°) | 12.6 (5.1) | 12.5 (5.1) | 12.41(4.7) |
| Time to peak internal rotation (sec) | 0.10 (0.03) | 0.10 (0.03) | 0.10 (0.03) |

354 * Significantly different to motion control

355 [†] Significantly different to neutral

356 Table 4. Comparison of hip joint kinematic parameters (mean (standard deviation)) in motion
 357 control, neutral and cushioned running shoes.

| | Motion Control | Neutral | Cushioned |
|---|----------------|-------------|-------------|
| X (+ = Flexion/ - = Extension) | | | |
| Angle at initial contact (°) | 25.2 (6.6) | 25.9 (7.0) | 25.3 (6.6) |
| Angle at toe off (°) | -7.2 (4.8) | -6.8 (5.2) | -7.6 (5.0) |
| Range of motion (°) | 33.9 (6.4) | 34.1 (6.6) | 34.3 (6.5) |
| Peak flexion (°) | 26.7 (6.1) | 27.3 (6.5) | 26.7 (6.1) |
| Time to peak flexion (sec) | 0.24 (0.03) | 0.23 (0.04) | 0.23 (0.03) |
| Y (+ = Adduction/ - = Abduction) | | | |
| Angle at initial contact (°) | 7.6 (4.5) | 7.1 (4.8) | 7.2 (4.5) |
| Angle at toe off (°) | 4.3 (4.3) | 4.1 (4.3) | 3.8 (4.4) |
| Range of motion (°) | 7.2 (3.7) | 7.0 (3.4) | 7.2 (3.9) |
| Peak adduction (°) | 11.0 (4.5) | 10.7 (4.7) | 10.6 (4.8) |
| Time to peak adduction (sec) | 0.07 (0.03) | 0.07 (0.04) | 0.08 (0.04) |
| Z (+ = Internal/ - = External) | | | |
| Angle at initial contact (°) | 3.2 (4.9) | 3.7 (5.0) | 3.2 (4.8) |
| Angle at toe off (°) | -2.6 (4.8) | -2.6 (5.0) | -3.2 (5.0) |
| Range of motion (°) | 7.7 (4.0) | 8.0 (3.6) | 8.1 (4.4) |
| Peak internal rotation (°) | 4.2 (4.8) | 04.5 (4.8) | 4.1 (4.7) |
| Time to peak internal rotation (sec) | 0.05 (0.08) | 0.06 (0.08) | 0.05 (0.07) |

358 * Significantly different to motion control

359 † Significantly different to neutral

360 **Figure Legends**

361

362 **Figure 1** – Lateral view of a participant’s lower leg and foot/shoe highlighting the rearfoot
363 technical marker placement, an additional technical cluster is visible and located at the midshaft
364 of the 5th metatarsal but was not utilised for this study

365

366 **Figure 2** - Stance phase hip, knee and ankle joint kinematics in motion control (solid grey line),
367 neutral (solid black line) and cushioned (dashed black line) running shoes, averaged across all
368 participants (n = 28)

369

Author Final Version