

Quantum-chemical analysis of the processes at the surfaces of Diesel fuel droplets

S.S. Sazhin^{1*}, V.M. Gun'ko^{2,1}, R. Nasiri¹

¹*Sir Harry Ricardo Laboratories, Centre for Automotive Engineering,
School of Computing, Engineering and Mathematics, University of Brighton, Brighton, BN2 4GJ, UK*

²*Chuiiko Institute of Surface Chemistry, 17 General Naumov Street, Kiev 03164 Ukraine*

Abstract

The quantum-chemical methods used for describing the processes at the surface of Diesel fuel droplets are summarised. Some results relevant to practical engineering application in Diesel engines, obtained previously, are summarised. Assuming that the droplets are so small that their interaction with individual molecules can be described using the methods of the kinetic gas theory (they can be considered as clusters/nanodrops), it was shown that the evaporation rate depends on partial pressures, temperature, and the sizes and masses of molecules and clusters/nanodrops. The results of the analysis of the collision processes between n-dodecane (approximation of Diesel fuel) molecules and clusters/nanodrops, based on the dynamic reaction coordinate (DRC) method, are described. It is concluded that the probability of the attacking molecule sticking to a droplet is maximal if the molecular plane is parallel or almost parallel to the droplet surface. If the kinetic energy of the attacking molecules is high (greater than that corresponding to the boiling temperature) then it is expected that it will scatter and be removed from the cluster/nanodrop surface. The mechanisms of evaporation of microdrops and nanodrops are shown to involve rather different processes. In the case of microdrops, individual C₁₂ molecules are evaporated from their surfaces, while in the case of nanodrops they can be disintegrated into clusters and individual molecules. The decrease in the likelihood of evaporation/condensation with temperature, predicted by the quantum-chemical (QC) approach, agrees with the prediction of the classical theory based on the MD simulations of n-dodecane molecules. The results of the estimation of the evaporation/condensation coefficient of n-dodecane molecules using the transition state theory (TST), based on the QC/DFT approach and taking into account the conformerisation of n-dodecane molecules, are summarised. It is shown that taking into account the QC effects leads to marginal modifications of the predicted evaporation/condensation coefficient, particularly at temperatures which are not close to the critical temperature.

Keywords:

Diesel fuel, Droplet evaporation, Gibbs free energy, Evaporation rate, Evaporation/condensation coefficient, Quantum chemical modelling

Nomenclature

b_{ij}	coefficient defined by Eq. (5)
E	Hamiltonian eigenvalue
G	Gibbs free energy
H	Hamiltonian operator
\hbar	reduced Planck constant
k_B	Boltzmann constant
m	mass
n	number of molecules
N	number of conformers
N_e	number of electrons in the system
p	pressure
$r_i; r_j$	radii of droplets or clusters
\mathbf{r}	position
R	universal gas constant
t	time or the duration of the process
T	temperature
V	potential energy

Greek symbols

β	evaporation coefficient
γ	evaporation rate
ρ	density
ψ	wave function

Subscripts

c	critical
e	electron
ev	evaporation
g	gas
l	liquid
0	initial

*Corresponding author. Tel. +44(0)1273642677; fax +44(0)1273642330; e-mail S.Sazhin@brighton.ac.uk

1. Introduction

The importance of the accurate modelling of the processes at the surfaces of Diesel fuel droplets is well recognised. These processes form integral parts of the processes of Diesel droplet heating and evaporation which precede the formation of the air/fuel vapour mixture and autoignition and combustion of this mixture in Diesel engines [1]. In almost all practical engineering approaches, the most basic models for these surface processes have been used. For example, it has been assumed that droplet convective heating can be adequately described by Newton's law of cooling, and Diesel fuel vapour in the vicinity of droplet surfaces has been assumed to be always saturated. The latter assumption has allowed the modellers to reduce the problem of droplet evaporation to a much simpler problem of fuel vapour diffusion from droplet surfaces to the ambient gas (see [2] for a detailed review of this approach, commonly known as hydrodynamic approach).

The limitations of the above-mentioned approach, however, have been widely recognised since the pioneering studies of these phenomena more than a century ago (see [3] for a review of early studies). It has been shown that even in the case when the processes of droplet heating and evaporation take place at high pressures, the conventional hydrodynamic approach to their modelling is no longer valid in the immediate vicinity of droplet surfaces. It has been suggested that in this region the processes of heat and mass transfer should be modelled based on the Boltzmann equations for species (kinetic approach). In a number of studies, including [4]-[9], the heating and evaporation of Diesel fuel (approximated by n-dodecane, $C_{12}H_{26}$) droplets has been analysed based on a model using a combination of the kinetic and hydrodynamic approaches. In the immediate vicinity of droplet surfaces (up to about one hundred mean molecular free paths), the vapour and ambient gas dynamics have been studied based on the Boltzmann equation or equations (kinetic region), while at larger distances the analysis has been based on the hydrodynamic equations (hydrodynamic region). One of the important limitations of the approaches described in [4]-[9] is that they were based on the assumption that Diesel fuel can be approximated by n-dodecane. A more detailed analysis of the composition of Diesel fuel has shown that it includes in the region of a hundred or more hydrocarbon components of various kinds [2, 10, 11].

It is not feasible to take into account the contributions of all these components in the kinetic modelling. At the same time, one can see that these components can be subdivided into two main groups: alkanes and aromatics [2]. The assumption that n-dodecane can approximate alkanes is widely used (see [10, 12, 13]), while aromatics could be approximated by p-dipropylbenzene [12]. In this case it has been suggested that a more accurate approximation of Diesel fuel, compared with the one based on its approximation by n-dodecane, could be its approximation by a mixture of n-dodecane and p-dipropylbenzene. The investigation

32 of the kinetic effects on heating and evaporation of two-component droplets (Diesel fuel was approximated
33 as a mixture of n-dodecane and p-dipropylbenzene) has been described in [14].

34 The solution to the Boltzmann equations in the kinetic region is based on the boundary conditions at
35 the surface of the droplet and at the interface between the kinetic and hydrodynamic regions. The boundary
36 conditions at the interface between the kinetic and hydrodynamic regions are commonly formulated as the
37 conservation of mass, momentum and energy fluxes at this interface. However, detailed knowledge of the
38 processes at the surface of the droplets is required to formulate the boundary condition at this region. In
39 most cases it has been assumed that the distribution function of the evaporating molecules is Maxwellian
40 and the values of the evaporation coefficient have been specified.

41 The most common approaches to estimating the value of the evaporation coefficient have been based on
42 molecular dynamic simulations. In [15, 16] these simulations have been performed based on the assumption
43 that Diesel fuel can be approximated by n-dodecane, and the structure of n-dodecane molecules has been
44 simplified assuming that the bonds between carbon and hydrogen atoms are much stronger than those
45 between carbon atoms, leading to the so called United Atom Model. It has been shown that the evaporation
46 coefficient of n-dodecane obtained using this approach increases with increasing temperatures and its values
47 are reasonably close to those estimated by other methods and for other substances. These values have been
48 used in the kinetic model for n-dodecane droplet evaporation described in [9]. Moreover, in [17] it has been
49 shown that the distribution function of molecules in the vicinity of the droplet surface can deviate from the
50 Maxwellian distribution, but this effect has not yet been taken into account in the kinetic modelling.

51 The main limitation of the model discussed in [15]-[17] is that in this model the interaction between
52 individual molecules was described within the force field (FF) methods, which simplify both inter- and
53 inner-molecular interactions by ignoring electrons *per se*. The applicability of this approach is far from
54 obvious, as the dynamics of individual molecules in the vicinity of droplet surfaces are essentially a quantum
55 mechanical process.

56 The quantum mechanical (quantum-chemical (QC)) models describing the processes at and in the vicinity
57 of Diesel fuel droplet surfaces are described in [11, 13, 18, 19]. These papers, however, primarily address the
58 quantum chemistry community. The importance of the results presented in these papers might have been
59 overlooked by a wider engineering audience. The main objective of the present paper is to summarise the
60 main results reported in the above-mentioned four papers, but in a format that can be easily understood by
61 the engineering community interested in modelling the heating and evaporation of Diesel fuel droplets.

62 The quantum-chemical methods used in the analysis and the compositions of Diesel fuel are discussed
63 in Sections 2 and 3, respectively. The results of the analyses, using several approximations, are described in
64 Section 4. The main results of the paper are summarised in Section 5.

2. Quantum-chemical methods of the analysis

Assuming that processes do not explicitly depend on time, the time independent Schrödinger equation for a single particle (electrons or nuclei) with potential energy V can be presented in the form

$$E\psi(\mathbf{r}) = -\frac{\hbar^2}{2m}\nabla^2\psi(\mathbf{r}) + V\psi(\mathbf{r}) \quad (1)$$

where E is the energy (Hamiltonian eigenvalue) including potential (electrons and nuclei) and kinetic (electrons) energy components, ψ is the wave function (the probability amplitude for the particle to be found at position \mathbf{r}), $H = -\frac{\hbar^2}{2m}\nabla^2 + V\psi$ is the Hamiltonian operator for a single particle, $-\frac{\hbar^2}{2m}\nabla^2$ is the kinetic operator, m is the mass of the particle, \hbar is the reduced Planck constant. The potential energy is determined by all particles (electrons and nuclei) in the system.

The solution to Eq. (1) in some simple cases (e.g. isolated hydrogen atom) is well known and described in standard quantum mechanics textbooks. The main difficulty emerges when Eq. (1) is applied to the case when many particles need to be analysed simultaneously, leading to the introduction of the multi-dimensional wave function:

$$\psi(\mathbf{r}_1, \mathbf{r}_2, \dots, \mathbf{r}_N).$$

An obvious simplification of the analysis of Eq. (1) in this case is based on the assumption that the analysis of dynamics of nuclei and electrons can be separated leading to the Born-Oppenheimer (adiabatic) approximation [20].

Further simplification of Eq. (1) for the electronic part of the wave function, ψ_e , could be based on the assumption that

$$\psi_e(\mathbf{r}_1, \mathbf{r}_2, \dots, \mathbf{r}_{N_e}) = \psi_{e1}(\mathbf{r}_1)\psi_{e2}(\mathbf{r}_2)\dots\psi_{eN_e}(\mathbf{r}_{N_e}).$$

This assumption was implicitly suggested by Hartree [21] almost 90 years ago and the modelling based on this assumption became known as the Hartree method. The wave function presented above, however, does not satisfy the Pauli principle as it does not change sign under the permutation of any pair of electrons. This problem was overcome by taking a linear combination of the functions $\psi_{ei}(\mathbf{r}_i)$ in the form of the Slater determinant [20]:

$$\psi_e(\mathbf{r}_1, \mathbf{r}_2, \dots, \mathbf{r}_{N_e}) = \frac{1}{\sqrt{N_e!}} \begin{vmatrix} \psi_{e1}(\mathbf{r}_1) & \psi_{e2}(\mathbf{r}_1) & \dots & \psi_{eN_e}(\mathbf{r}_1) \\ \psi_{e1}(\mathbf{r}_2) & \psi_{e2}(\mathbf{r}_2) & \dots & \psi_{eN_e}(\mathbf{r}_2) \\ \dots & \dots & \dots & \dots \\ \dots & \dots & \dots & \dots \\ \psi_{e1}(\mathbf{r}_{N_e}) & \psi_{e2}(\mathbf{r}_{N_e}) & \dots & \psi_{eN_e}(\mathbf{r}_{N_e}) \end{vmatrix} \quad (2)$$

Factor $1/\sqrt{N_e!}$ ensures that the wave function is normalised if the components $\psi_{ei}(\mathbf{r}_i)$ are normalised. The value of each component for a given electron is found based on the assumption that the mean field produced

83 by all other electrons is known. This leads to the need for the iterative processes leading to the calculation of
84 the self-consistent field. This method was sometimes called the self-consistent field (SCF) method, although
85 nowadays it is commonly known as the **Hartree-Fock (HF) method** (see [20] for further details).

86 There are two strategies for application of the HF method for practical calculations [20]. In the **semi-**
87 **empirical methods** the integrals used in the HF method are estimated based on experimental data or
88 based on a series of rules which allow us to set certain integrals to zero. In the *ab initio* methods an attempt
89 is made to calculate all these integrals.

90 Although the Hartree-Fock method is widely used in practical computations, this method is still an
91 approximate one and demands considerable computational effort. This led to the development of alternative
92 approaches to the calculation of electronic systems. The technique which gained considerable ground recently
93 is known as the **Density Functional Theory (DFT)** [20]. This technique is focused on the electron density
94 (ρ_e) rather than on the wave function ψ_e . Hence the term ‘density’ in the name of the theory. In this theory
95 it is assumed that the energy of a molecule is a function of the electron density. Since the electron density
96 is the function of position $\rho_e(\mathbf{r})$, this energy appears to be the function of the function, that is functional
97 of density. This approach appears to be not only much less demanding computationally compared with the
98 HF method, but in some cases it can lead to more accurate results compared with the latter method.

99 On some occasions various approximations of the energy functional in the DFT, that incorporate parts
100 of the exact exchange from the HF theory, have been suggested. One such approach is known as **B3LYP**,
101 which stands for Becke, 3-parameter, Lee-Yang-Parr, and the exchange-correlation energy functional.

102 Various semi-empirical quantum chemistry methods, mentioned earlier, are important for dealing with
103 large molecules where the full Hartree-Fock method without the approximations (*ab initio* approach) and
104 DFT are too expensive. In these methods a range of fitting parameters are typically used to produce the
105 results that best agree with experimental data or with *ab initio* results. One of these methods is known as
106 the **PM7** method.

107 The parameters in the PM7 method were calibrated to obtain results consistent with experimental and
108 *ab initio* data for more than 9000 compounds [22, 23]. This method can be used to study properties of
109 compounds (molecules, polymers, and solids with up to 83 chemical elements), including thermodynamic
110 properties (heat of formation, entropy, free energy, heat capacity). It is characterised by its average unsigned
111 error (AUE) which is close to that of B3LYP/6-31G(d) and HF/6-31G(d) [22, 23]. As a whole, it gives the
112 best results for a large variety of organic and inorganic compounds among other semi-empirical QCMs
113 [22, 23]. The main differences between the classical MM/MD, semi-empirical PM7, *ab initio* and DFT
114 methods [24, 26] are due to the way in which the contributions of electrons are taken into account. The
115 contribution of all electrons is taken into account in *ab initio* and DFT with SCF; only valence electrons are
116 considered in semi-empirical QCMs with SCF, and no electrons *per se* are considered in classical MM/MD
117 methods without SCF [24, 25, 26]. The accuracy of *ab initio* molecular orbital (MO) computations depends

118 on the atomic orbital (AO) basis set for all electrons of atoms in molecules. These computations use
119 the fundamental constants, as well as the mass and charge of the nuclear particles from experiments or
120 Hartree-Fock (HF) approximations [24, 27, 25]. The electronic structure of molecules is described in MO
121 computations as linear combinations of the AOs (MOLCAO approach) within the SCF [24]. The 6-31G(d,p)
122 basis set has been selected as a minimal appropriate basis set to analyse the evaporation of Diesel fuel droplets
123 [11]. Note that the accuracy of the PM7 method is close to that of the *ab initio* and DFT methods used
124 with the 6-31G(d) basis set [22, 23].

125 A new continuum solvation model based on the quantum mechanical charge density of a solute molecule
126 interacting with a continuum description of a solvent was suggested in [28]. This solvation model was called
127 **SMD**, where *D* stands for density which refers to the full solute electron density (without defining partial
128 atomic charges). The term continuum indicates that the solvent is represented as a dielectric medium with
129 surface tension at the solute-solvent boundary. The model separates the observable solvation free energy
130 into two main components. The first component is the bulk electrostatic contribution arising from a self-
131 consistent reaction field treatment that involves the solution of the nonhomogeneous Poisson equation for
132 electrostatics. The second component was called the cavity-dispersion-solvent-structure term and referred to
133 the contribution arising from short-range interactions between the solute and solvent molecules in the first
134 solvation shell. The SMD model was parameterized with a training set of almost three thousand solvation
135 data.

136 In the case of modelling of the transient processes, the **Dynamic Reaction Coordinates (DRC)**
137 method is widely used [29]. The key concept of this method is the Dynamic Reaction Coordinate which
138 is the path followed by all the atoms in a system assuming the conservation of energy. In contrast to
139 conventional molecular dynamic (MD) approaches, the contributions of the processes at the electronic level
140 are taken into account.

141 The models mentioned above have been implemented in a number of known programs. In our analysis
142 we used mainly Gaussian 09, WinGAMESS 2013 R1, and MOPAC2012.

143 **3. Composition of Diesel fuel**

144 Real-life Diesel fuel, the composition of which is described in [11, 2], was used in the analysis of [11, 13].
145 Molar fractions of various compounds in this fuel are the following: 13.7% paraffins, 26.4% isoparaffins, 14.9,
146 7.6, and 1.6% mono-, bi- and tri-cyclic alkanes, respectively, 16.2% alkylbenzenes, 9.2% indanes and tetra-
147 lines, 8.7% naphthalenes, and small amounts of other compounds. To approximate this composition, a set of
148 representative compounds was selected, including: normal alkanes – n-octane, n-dodecane, n-didecyl, and n-
149 heptacosane; isoalkanes – 3,6,9,10-methyl-dodecane; cycloalkanes – 1-propyl-3-hexyl-cycloheptane, diethylbi-
150 cycloheptane, and ethylcycloheptane cyclononane; and aromatics – 1,4-dipropylbenzene, 1,4-dipentylbenzene,

151 pentylindane, 1-propylnaphthalene, di(3-ethyl-phenyl)methane, 1-propyl-(1,2,3,4-tetrahydronaphthalene),
152 1-pentyl-(1,2,3,4-tetrahydronaphthalene), and ethylphenanthrene.

153 In some cases, a simplified approximation of Diesel fuel by alkanes or even n-dodecane have been used,
154 although the limitations of this approach are well known (e.g. [2]).

155 4. Results

156 4.1. Evaporation rate

157 To the best of our knowledge, the first attempt to perform a quantum chemical study of the processes
158 during the evaporation of real-life Diesel fuel droplets was described in [11]. The analysis of that paper
159 was focused on the evaporation from the surface of a Diesel fuel droplet into a vacuum, described by the
160 evaporation rate determined by the equation:

$$\gamma = \left(\frac{1}{t}\right) \ln \left(\frac{n_{\text{ev}}(t)}{n_0}\right), \quad (3)$$

161 where $n_{\text{ev}}(t)$ is the time dependent number of molecules leaving the droplet, n_0 is the initial number of
162 molecules, t is the duration of the process. Quantitative estimation of γ was based on the following formula,
163 derived by Ortega et al. [30, 31]:

$$\gamma_{i(i+j)} = b_{ij} \frac{p}{k_B T n_0} \exp \left(\frac{\Delta G_{i+j} - \Delta G_i - \Delta G_j}{k_B T} \right), \quad (4)$$

164 where $\gamma_{i(i+j)}$ is the evaporation rate of the i th-molecule from a cluster (or nanodrop) $i+j$, b_{ij} is the collision
165 rate of the i th molecule with the j th cluster or nanodrop, ΔG_{i+j} , ΔG_i , and ΔG_j are the Gibbs free energies
166 of formation of the molecules (clusters/nanodrops) from monomers (molecules) at the reference pressure p .

167 To estimate b_{ij} an additional assumption was made that clusters or nanodrops are so small that their
168 interaction with molecules can be described by the kinetic gas theory. In this case, the value of b_{ij} can be
169 inferred from the following expression [30, 31, 32]:

$$b_{ij} = \frac{1}{\sqrt{8\pi k_B T}} \left(\frac{1}{m_i} + \frac{1}{m_j} \right)^{1/2} (r_i + r_j)^2, \quad (5)$$

170 where m_i and m_j are the masses of the i th molecule and j th molecule/cluster/nanodrop, r_i and r_j are their
171 radii.

172 Although the above-mentioned assumptions are rather restrictive for practical engineering applications,
173 they allowed the authors of [11] to clarify the underlying physics of some of the processes at the surface of
174 the droplets. The SMD/HF or SMD/DFT with the same 6-31G(d,p) basis set were used in [11] to estimate
175 changes in the Gibbs free energy during the transfer of a molecule from a liquid medium into a gas phase.
176 It was shown that the evaporation rate depends on partial pressures, temperature, sizes and masses of
177 molecules and clusters/nanodrops. Such solvents as n-dodecane, tetraline, benzene, and isopropyltoluene

178 were used to analyse the effects of surroundings on the evaporation rate of the components of Diesel fuel:
179 normal, iso and cyclic alkanes, 1-3 ring aromatics, tetralines and indanes (in the C_{12} - C_{20} range). It was
180 shown that compounds C_{14} - C_{16} make the main contribution to the Diesel fuel under consideration; all cyclic
181 organics have the C_1 - C_6 aliphatic side groups. An increase in the molecular size of alkanes from n-octane
182 to n-heptacosane or in the aromaticity of compounds resulted in a strong decrease in the values of the
183 evaporation rate.

184 The processes considered in [11] were further investigated in [13]. In contrast to [11], the analysis of [13]
185 was focused only on alkanes as the main components of Diesel fuels, and particularly on n-dodecane, the
186 component widely used as a representative of this fuel. The analysis of [13] was based on the assumption
187 that the system is in a state of thermodynamic equilibrium (evaporation and condensation rates are equal).
188 The evaporation rate was shown to decrease with increasing cluster/nanodrop diameter and decreasing
189 temperature. The relative number of evaporated molecules, however, does not depend on cluster/nanodrop
190 diameters, and increases with increasing temperature. At certain temperatures, the clusters/nanodrops were
191 expected to fully evaporate. The relative number of residual molecules in clusters/nanodrops for n-alkanes
192 in the range C_8 - C_{27} was shown to increase with temperature and with the carbon numbers in the molecules.
193 Thus the evaporation process of a mixture of n-alkanes was expected to lead to increased concentration
194 of heavy n-alkanes in droplets. This result is consistent with the one inferred from classical analyses of
195 multi-component droplet heating and evaporation (e.g. [2]).

196 *4.2. Interaction between molecules and clusters/nanodrops*

197 The analysis described so far in this section was focused on the average or integral characteristics of the
198 processes at the surface of the droplets. In what follows, the details of the analysis of the collision processes
199 between n-dodecane molecules and clusters/nanodrops are described, following [13]. The analysis of that
200 paper was based on the Dynamic Reaction Coordinate (DRC) method. The application of this method allows
201 one to elucidate the interaction mechanism of a molecule with a cluster/nanodrop depending on the kinetic
202 characteristics and temperature of the system. The characteristics of this mechanism refer to scattering or
203 sticking of the molecules. In the DRC calculations, the total kinetic energy is partitioned into the kinetic
204 energy of random thermal bond vibrations and rotations and the kinetic energy of the translational motion
205 of the whole molecules. In [13], the DRC method was applied to study the dependence of sticking/scattering
206 of n-dodecane molecules on their angles of attack, kinetic energy (temperature), and cluster/nanodrop size.
207 The DRC calculations were performed for molecules interacting with a cluster (7 molecules) or a nanodrop
208 (64 or 128 molecules) of n-dodecane molecules. The results are shown in Figs. 1 and 2. The information
209 presented in these figures is similar to that presented in Figs. 5 and 7 of [13].

210 As one can see from Figs. 1, at large angles of attack, a molecule is absorbed by a cluster or nanodrop
211 of relatively small size ($d = 2$ - 7 nm) if the kinetic energy is low and the attacking molecule is not oriented

212 exactly towards one of the surface molecules (but rather between neighbouring surface molecules) (see Fig.
213 1b). At $\Theta \approx 1^\circ$ (see Fig. 1a) an almost perfectly elastic collision was observed if the molecule had relatively
214 high velocity (kinetic energy ~ 10 kJ/mol or larger) and was oriented directly towards one of the surface
215 molecules. In the DRC calculations shown in Figs. 1, the kinetic energy of the molecules in the clusters or
216 nanodrops was low and thermal vibrations and bond rotations corresponded to 300-400 K. At the same time,
217 the kinetic energy of the attacking molecule was high (its effective temperature was in the range 500-1200
218 K). In Fig. 2, the results of calculations for larger systems, using the PM7 method, are shown.

219 Although the clusters and nanodrops shown in Figs. 1 and 2 are not particularly good approximations
220 of fuel droplets in real-life Diesel engine conditions, the results of our analysis allowed us to identify the
221 correct underlying physics of the droplet evaporation/condensation processes which is generally overlooked
222 when the conventional methods of the analysis of the phenomena are applied.

223 Further analyses, similar to those shown in Figs. 1 and 2, allowed the authors of [13] to conclude that
224 the probability of the attacking molecule sticking to a droplet is maximal if the molecular plane is parallel
225 or almost parallel to the droplet surface as this corresponds to multi-point interactions of relatively long
226 n-dodecane molecules with the droplet surface. If the kinetic energy of the attacking molecules is high
227 (greater than that corresponding to boiling temperature) then it is expected that they will scatter and be
228 removed from the cluster/nanodrop surface. Molecule-nanodrop interaction results (sticking or scattering)
229 depend on the kinetic energy and orientations of the attacking and surface molecules. It was shown that
230 the mechanisms of evaporation of microdrops and nanodrops are likely to involve rather different processes.
231 In the case of microdrops, individual C_{12} molecules are evaporated from their surfaces, while in the case of
232 nanodrops they can be disintegrated into clusters and individual molecules.

233 It was shown that the decrease in the likelihood of evaporation/condensation with temperature, pre-
234 dicted by the analysis presented above, agrees with the prediction of the classical theory based on the
235 MD simulations of n-dodecane molecules (see [15, 16, 17]). At the same time, the analysis presented in
236 this section does not allow us to predict the evaporation coefficient, as was done in [15, 16, 17]) using the
237 classical FF analysis. The analysis of each collision process, similar to the ones shown in Fig. 1, required
238 a powerful PC (three four-core PCs with a chip Core i7 were used for two-month calculations of a small
239 systems with eight n-dodecane molecules). To study these processes using DFT/DRC methods for larger
240 systems with dozens or hundreds of the molecules, a supercomputer would be needed. The latter was used
241 for some calculations to study the conformerisation effects for n-dodecane (95 conformers). To quantify
242 the values of the evaporation/condensation coefficient, using the above-mentioned analysis, one would need
243 to repeat these calculations for a wide range of the angles of attack, orientation of molecules and energies
244 for various conformers (cf. [19]) and various conditions of clusters and nanodrops (the effects of the size
245 of the clusters/nanodrops would need to be investigated as well). Since this does not look feasible at the
246 moment, an alternative approach to calculating the above-mentioned evaporation/condensation coefficient,

247 taking into account quantum chemical effects, is described in the next section, following [18].

248 4.3. Estimation of the evaporation/condensation coefficient

249 The analysis of [18] was based on the transition state theory (TST) and quantum chemical DFT methods.
250 These were applied to several ensembles of conformers of n-dodecane molecules. There was some similarity
251 between the approach used in [18] and the one used previously (see [1]). In contrast to the previous
252 studies, however, in the analysis of [18] the TST was based on a QC DFT approach taking into account
253 the conformerisation of n-dodecane molecules. As in many previous studies, n-dodecane was considered as
254 a representative of Diesel fuel (see [2] for the analysis of the validity of this assumption).

255 Several approaches to the estimation of the evaporation/condensation coefficient β were considered in
256 [18]. It was shown that the most accurate expression for the condensation coefficient is the one averaged
257 over the states of various conformers transferred between two phases and given by the following formula:

$$\langle \beta_V \rangle = \left\{ 1 - \left[\frac{\rho_g}{\rho_l} \exp \frac{\langle \Delta G_{g \rightarrow l} \rangle}{RT} \right]^{1/3} \right\} \exp \left\{ -0.5 \left[\left[\frac{\rho_g}{\rho_l} \exp \frac{\langle \Delta G_{g \rightarrow l} \rangle}{RT} \right]^{1/3} - 1 \right]^{-1} \right\}, \quad (6)$$

258 where R is the universal gas constant, $\rho_{g(l)}$ is the gas (liquid) density, $\Delta G_{g \rightarrow l}$ is the change in the Gibbs free
259 energy during the condensation process, subscript V indicates that the expression for β explicitly depends
260 on the specific volumes, $\langle \rangle$ indicates averaging over the states of various conformers transferred between
261 two phases. It is assumed that the process under consideration is quasi-steady-state and the condensation
262 coefficient predicted by Eq. (6) is equal to the evaporation coefficient.

263 The effects of both the conformerisation and cross-conformerisation (changes in conformer state during
264 transfer into another phase) of n-dodecane molecules (CDM effects), which can contribute to the Gibbs free
265 energies of evaporation and solvation, were analysed using the MSTor program [33, 34] applied to n-dodecane
266 at 300-1200 K. Ninety-five stable conformers were selected based on the changes in the Gibbs free energy
267 from 1000 conformers generated by ConfGen [33]. The results of calculations for these conformers are shown
268 in Table 1. The numbers referring to conformers under consideration were random and do not depend on the
269 value of G . This was done to obtain a relatively random set of conformers at various $N \leq 95$ characterised
270 by wide distributions of the values of G . Details of the calculations are given in the supplementary material
271 of [18].

272 Note that Table 1 is slightly different from the corresponding table presented in [18], where the results
273 of calculations were presented only for 73 out of 95 conformers. This difference, however, did not lead to
274 any difference in the conclusions (see Fig. S2 of [18]).

275 A comparison between the results of calculations of β based on Expression (6) and those obtained
276 previously is shown in Fig. 3. Some of the results presented in this figure are reproduced from Fig. 5 of
277 [18]. As one can see from this figure, taking into account the QC effects leads to marginal modifications of

278 the predicted evaporation/condensation coefficient, except at temperatures close to the critical temperature
279 (where this modification turned out to be significant). Thus, although the analysis of the QC effects takes
280 into account many new effects ignored in the conventional FF approach, the contribution of these effects to
281 the values of the evaporation/condensation coefficient turned out to be marginal, unless temperatures close
282 to the critical temperature were considered.

283 5. Conclusions

284 The quantum mechanical (quantum-chemical) methods, used for describing the processes at Diesel fuel
285 droplet surfaces, are summarised. These methods include the Hartree-Fock (HF) method, the Density Func-
286 tional Theory (DFT), the PM7 method, the solvation model SMD, and the Dynamic Reaction Coordinates
287 (DRC) method. Diesel fuel with the following molar fractions of compounds was used in the analysis: 13.7%
288 paraffins, 26.4% isoparaffins, 14.9, 7.6, and 1.6% mono-, bi- and tri-cyclic alkanes, respectively, 16.2% alkyl-
289 benzenes, 9.2% indanes and tetralines, 8.7% naphthalenes, and small amounts of other compounds. On some
290 occasions this composition was simplified to the approximation of Diesel fuel by alkanes or even n-dodecane.

291 Some results relevant to practical engineering applications in Diesel engines, obtained previously, are
292 summarised. Assuming that the droplets are so small that their interaction with individual molecules can
293 be described using the methods of the kinetic gas theory (they can be considered as clusters/nanodrops), it
294 was shown that the evaporation rate depends on partial pressures, temperature, sizes and masses of molecules
295 and clusters/nanodrops. Also, it was shown that compounds C_{14} - C_{16} make the main contribution to the
296 Diesel fuel under consideration. An increase in the molecular size of alkanes from n-octane to n-heptacosane
297 or in the aromaticity of compounds resulted in a strong decrease in the values of the evaporation rate. The
298 evaporation process of a mixture of n-alkanes was shown to lead to an increased concentration of heavy
299 n-alkanes in droplets.

300 The results of the analysis of the collision processes between n-dodecane (approximation of Diesel fuel)
301 molecules and clusters/nanodrops, based on the Dynamic Reaction Coordinate (DRC) method, are sum-
302 marised. In the DRC calculations, the total kinetic energy is partitioned into the kinetic energy of ran-
303 dom thermal bond vibrations and rotations and the kinetic energy of the translational motion of the whole
304 molecules. This approach was applied to study the dependence of sticking/scattering of n-dodecane molecules
305 on their angles of attack, kinetic energy (temperature), and cluster/nanodrop size.

306 It was concluded that the probability of the attacking molecule sticking to a droplet is maximal if
307 the molecular plane is parallel or almost parallel to the droplet surface as this corresponds to multi-point
308 interactions of relatively long n-dodecane molecules with the droplet surface. If the kinetic energy of the
309 attacking molecules is high (greater than that corresponding to the boiling temperature) then it is expected
310 that they will scatter and be removed from the cluster/nanodrop surface. Molecule-nanodrop interaction

311 results (sticking or scattering) depend on the kinetic energy and orientations of the attacking and surface
312 molecules. It was shown that the mechanisms of evaporation of microdrops and nanodrops are likely to
313 involve rather different processes. In the case of microdrops, individual C₁₂ molecules are evaporated from
314 their surfaces, while in the case of nanodrops they can be disintegrated into clusters and individual molecules.
315 It was shown that the decrease in the likelihood of evaporation/condensation with temperature agrees with
316 the prediction of the classical theory based on the MD simulations of n-dodecane molecules.

317 The results of the estimation of the evaporation/condensation coefficient of n-dodecane molecules using
318 the TST, based on the QC DFT approach, and taking into account the conformerisation of n-dodecane
319 molecules, are summarised. It was shown that taking into account the QC effects leads to marginal modi-
320 fications of the predicted evaporation/condensation coefficient, particularly at temperatures which are not
321 close to the critical temperature. Thus, although the analysis of the QC effects takes into account many
322 new processes ignored in the conventional approach, the contribution of these effects to the values of the
323 evaporation/condensation coefficient turns out to be marginal.

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398 Figure Captions

399

400 **Fig. 1** Interaction of an n-dodecane molecule (hot, temperature ~ 1100 K) with a cluster of seven n-
 401 dodecane molecules (initial temperature 473 K; it increases due to the interaction with a hot molecule) at
 402 the angles of attack $\Theta \approx$ (a) 1° , (b) 60° and (c) 90° . The results were obtained using the DFT B3LYP.

403

404 **Fig. 2** Changes in the kinetic energy of the attacking n-dodecane molecule during its interaction with a
 405 nanodroplet of 64 n-dodecane molecules at various angles of attack: (a) 5° , (b) 40° , and (c) 45° , and two ini-
 406 tial kinetic energies: (a, b) 125.5, (c) 1602 kJ/mol (these kinetic energies correspond to the energies of both
 407 translational motion and thermal vibrations or rotations). The results were obtained using the PM7 method.

408

409 **Fig. 3** Comparison of the values of the evaporation coefficient β , predicted by MD FF (symbols 1-4,
 410 curves 5-8) and Expression (6) (curve 9), versus normalised temperature (T/T_c , where T_c is the critical
 411 temperature). Symbols (1-4) refer to the models for structureless LJ fluids with various input parameters
 412 [35, 36], curves 5 and 7 refer to the results obtained based on the United Atom Model reported in [15, 16],
 413 respectively, curve 6 refers to the results of calculations based on the TST model reproduced from [15], curve
 414 8 is based on the results of calculations using the model described by Mizuguchi et al. [30]. QC calculations
 415 were performed using DFT ω B97X-D/cc-pVTZ and SMD/ ω B97X-D/cc-pVTZ.

416

417

418 Table Captions

419

420 **Table 1** Sums of electronic and thermal Gibbs free energies in Hartrees (1 Ha = 627.5 kcal/mol) for
 421 n-dodecane conformers in the gas (ω B97X-D/cc-pVTZ) and liquid (SMD/ ω B97X-D/cc-pVTZ) phases.

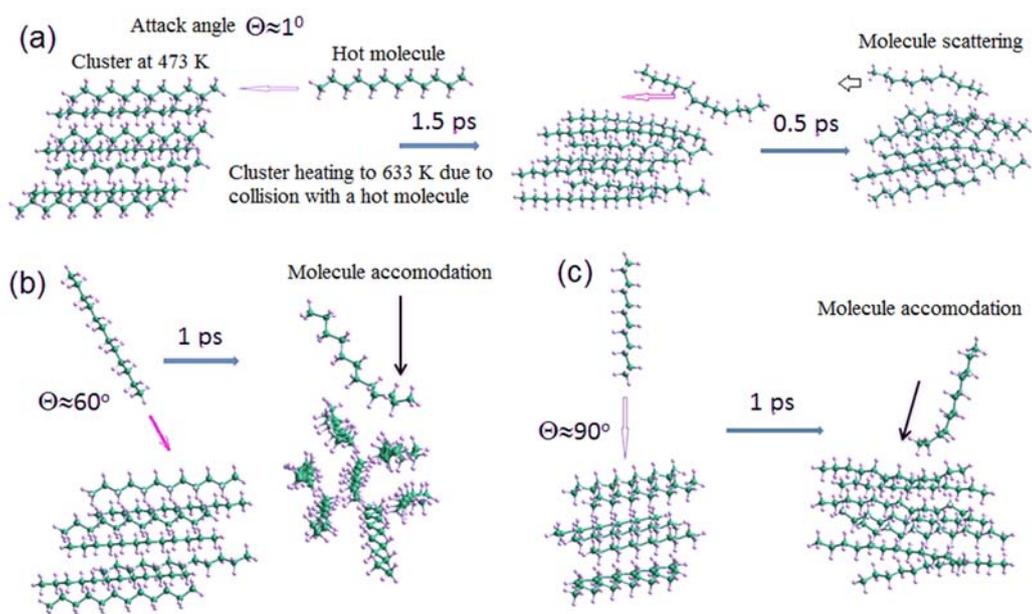


Fig. 1

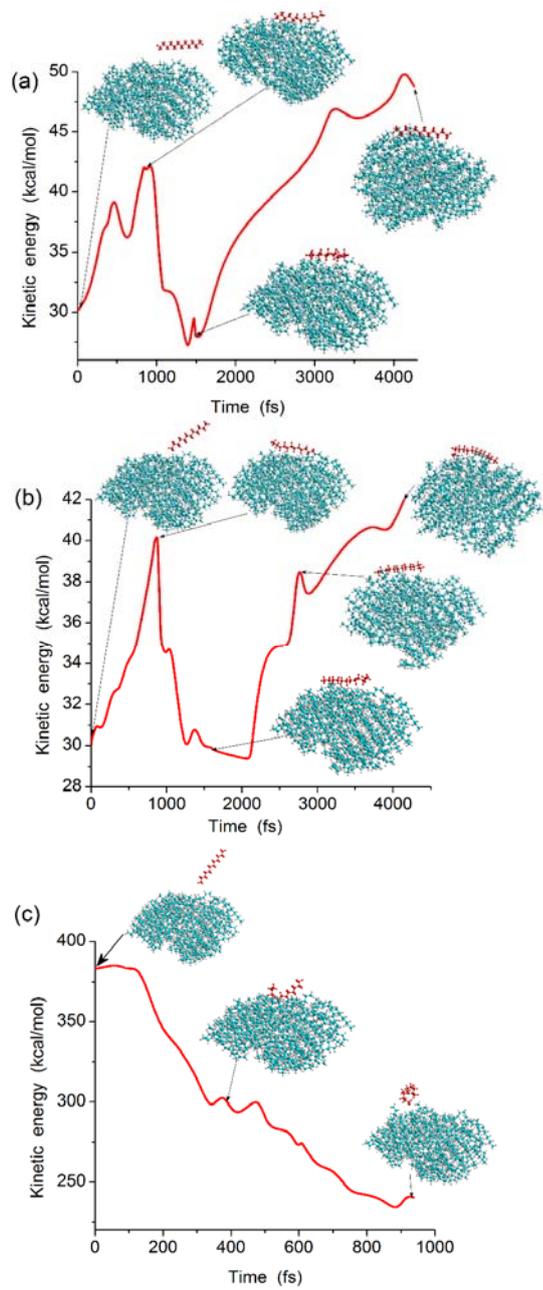


Fig. 2

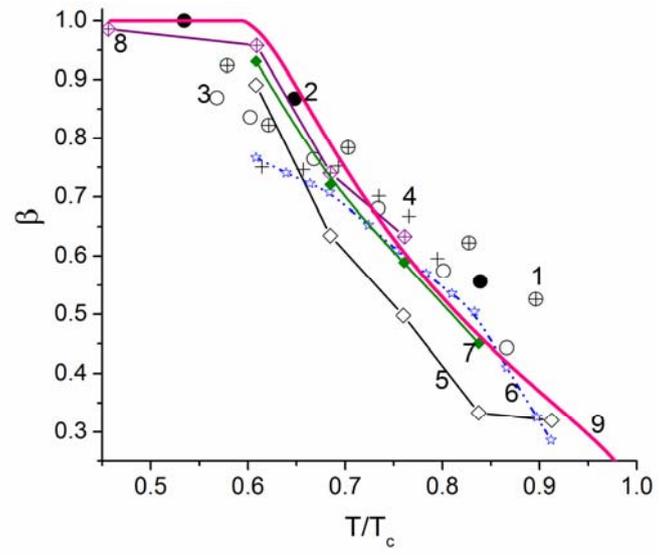


Fig. 3

Table 1. Sum of electronic and thermal Gibbs free energies for *n*-dodecane conformers in the gas (ω B97X-D/cc-pVTZ) and liquid (SMD/ ω B97X-D/cc-pVTZ) phases.

Conformer	Free energy, gas (Ha)	Free energy, liquid (Ha)	Conformer	Free energy, gas (Ha)	Free energy, liquid (Ha)	Conformer	Free energy, gas (Ha)	Free energy, liquid (Ha)
1	-472.672861	-472.683897	33	-472.666819	-472.677786	65	-472.668277	-472.679477
2	-472.671955	-472.683668	34	-472.667748	-472.678665	66	-472.670404	-472.681027
3	-472.673521	-472.684762	35	-472.675919	-472.683376	67	-472.670459	-472.679261
4	-472.669991	-472.681439	36	-472.671182	-472.682571	68	-472.668546	-472.679797
5	-472.673067	-472.685107	37	-472.671964	-472.681410	69	-472.670770	-472.679867
6	-472.671544	-472.683589	38	-472.668438	-472.679998	70	-472.669831	-472.681039
7	-472.672687	-472.680659	39	-472.671322	-472.682050	71	-472.666341	-472.677079
8	-472.672774	-472.684828	40	-472.669002	-472.680389	72	-472.669850	-472.680589
9	-472.673212	-472.686184	41	-472.671980	-472.683730	73	-472.667851	-472.669995
10	-472.669906	-472.681049	42	-472.670167	-472.679637	74	-472.668430	-472.679420
11	-472.669804	-472.679133	43	-472.673422	-472.680413	75	-472.666560	-472.677692
12	-472.675212	-472.685893	44	-472.672426	-472.680146	76	-472.666759	-472.678866
13	-472.672504	-472.681944	45	-472.671954	-472.682834	77	-472.667940	-472.679737
14	-472.671916	-472.683465	46	-472.669203	-472.679901	78	-472.667880	-472.678390
15	-472.671710	-472.682647	47	-472.669624	-472.677674	79	-472.668777	-472.680167
16	-472.670279	-472.679715	48	-472.667998	-472.678862	80	-472.666489	-472.677570
17	-472.669692	-472.681345	49	-472.672894	-472.683414	81	-472.669385	-472.677278
18	-472.667835	-472.678967	50	-472.673155	-472.683309	82	-472.667478	-472.677968
19	-472.669889	-472.680603	51	-472.668302	-472.679393	83	-472.666826	-472.677891
20	-472.671695	-472.684512	52	-472.666487	-472.677630	84	-472.663619	-472.674752
21	-472.672225	-472.683415	53	-472.668599	-472.680286	85	-472.668170	-472.677190
22	-472.668706	-472.679769	54	-472.670937	-472.683122	86	-472.664836	-472.676118
23	-472.671085	-472.682521	55	-472.670226	-472.677905	87	-472.667376	-472.678708
24	-472.669610	-472.680499	56	-472.671101	-472.680866	88	-472.667298	-472.678691
25	-472.667748	-472.678665	57	-472.683570	-472.671654	89	-472.666980	-472.678400
26	-472.670753	-472.679134	58	-472.672047	-472.682414	90	-472.664286	-472.674884
27	-472.668744	-472.681313	59	-472.670564	-472.681625	91	-472.665538	-472.676583
28	-472.669767	-472.681307	60	-472.670052	-472.681207	92	-472.671255	-472.683714
29	-472.666725	-472.677911	61	-472.672385	-472.684404	93	-472.671323	-472.682050
30	-472.670599	-472.677483	62	-472.669508	-472.679963	94	-472.664719	-472.675590
31	-472.669418	-472.680500	63	-472.670850	-472.681636	95	-472.666980	-472.678400
32	-472.664644	-472.676310	64	-472.668540	-472.679033			